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Simple Design of a Tunable Quadruple-Broadband Terahertz Metamaterial Absorber Based on VO_2

Kwang-Jin Ri[1, *], Dae-Song Pak[2], Chung-Ho Ri[1]

[1]Department of Physics, University of Sciences, Pyongyang, Democratic People's Republic of Korea

[2]Department of Physics, Kim Hyong Jik University of Education, Pyongyang, Democratic People's Republic of Korea

Email address:

rkj1994@star-co.net.kp (Kwang Jin Ri)

[*]Corresponding author

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Abstract: Tunable multi-broadband terahertz (THz) metamaterial absorbers (MAs) can effectively act as THz amplitude modulators, which are the essential components for the future THz communication systems. Till now, various tunable multi-broadband THz MAs including tunable dual-broadband and triple-broadband absorbers have been investigated. However, there are few researches on tunable quadruple-broadband THz MAs. In this work, a simple design of tunable quadruple-broadband THz MA based on VO_2 is proposed. The proposed absorber possesses four broad absorption bands with absorptivity over 90% in frequency ranges of 0.54-2.30 THz, 3.67-5.33 THz, 6.72-8.4 THz and 9.72-11.47 THz, and the corresponding absorption bandwidths reach 1.76 THz, 1.66 THz, 1.68 THz and 1.75 THz, respectively. Moreover, we can dynamically control the absorptivity of four absorption bands by varying VO_2 conductivity. Thus, the proposed absorber possesses the modulation depths of 79.15%, 49.71%, 33.03% and 21.98% at 1.48 THz, 4.46 THz, 7.45 THz and 10.44 THz, respectively. The physical origin of quadruple-broadband perfect absorption is revealed with aid of electric field distributions at resonant frequencies. We also investigate the effects of incidence angle and polarization angle on the quadruple-broadband perfect absorption. The proposed absorber has broad application prospects in THz imaging, modulating, detecting and sensing owing to its excellent absorption characteristics.

Keywords: Terahertz, Metamaterial, Quadruple, Tunable, Vanadium Dioxide, Bandwidth

1. Introduction

Today, THz technology has been widely introduced in 5G, 6G communication [1], security [2], biomedicine [3] and nondestructive detection [4]. Particularly, THz MAs have drawn more and more attention because of their critical roles in many THz functional devices. In 2008, Tao and his colleagues [5] firstly proposed the narrowband THz MA. Thereafter, a great number of THz MAs have been developed to obtain multi-band and broadband perfect absorptions [6-16]. However, these MAs are designed and fabricated mainly by using the metal-dielectric-metal structure. Such a configuration unavoidably results in the difficulty in controlling the absorption performances. In fact, the preferred MAs for practical application fields are tunable THz MAs.

Over the past years, tunable THz MAs based on active materials [17-27] have achieved tremendous progress. Particularly, many researchers have investigated VO_2-based tunable broadband THz MAs [28-35]. Meanwhile, recently, many efforts have been focused on the design of tunable multi-broadband THz MAs. In future, THz communication systems will require the tunable multi-broadband THz MAs to promote multi-task systems [36]. Moreover, these absorbers are also very useful for sensing applications [37]. In 2020, a tunable dual-broadband THz MA using VO_2 material was designed and investigated by Jiao et al. [38]. This absorber has two broad absorption bands with absorptivity over 90% in frequency ranges of 1.87 THz-4.19 THz and 8.70 THz-10.73 THz, and its absorptivity can be dynamically changed between 2% and 94%. Huang et al. [39] designed an active controllable dual-broadband THz MA with VO_2 resonator, the absorption bandwidths of 80% absorptivity are 0.88 THz and 0.77 THz. Moreover, its

absorptivity can be adjusted from 20% to 90%. In 2022, Feng et al. [40] designed a tunable dual-broadband THz MA based on VO_2 material. The absorption bandwidths of 90% absorptivity are 3.4 THz and 3.06 THz, and its absorptivity can be changed from 2% to 100%. In 2023, Ri et al. [41] designed a tunable dual-broadband THz MA with slotted VO_2 resonator, the absorption bandwidths of 90% absorptivity can reach 3.41 THz and 3.25 THz. In addition, its absorptivity can be changed from 20% to over 90%. In the latest work [42], a novel tunable triple-broadband THz MA with single VO_2 ring was proposed, the absorption bandwidths of 90% absorptivity were 2.35 THz, 2.30 THz and 2.40 THz, and the absorptivity can be dynamically changed from 20% to over 90%. However, recent researches on tunable multi-broadband MAs are mainly limited to the tunable dual-broadband and triple-broadband THz MAs, no further research on tunable quadruple-broadband THz MA has been carried out.

In this work, we propose a novel tunable quadruple-broadband THz MA with single VO_2 resonator, whose absorptivity exceeds 90% in the four frequency ranges of 0.54-2.30 THz, 3.67-5.33 THz, 6.72-8.4 THz and 9.72-11.47 THz, and the corresponding absorption bandwidths are 1.76 THz, 1.66 THz, 1.68 THz and 1.75 THz, respectively. Compared with previous tunable multi-broadband THz absorbers, our designed absorber has the excellent characteristics of quadruple-band, broadband, and simple resonant structure. Moreover, the absorptivity of four absorption bands can be continuously adjusted under thermal control. The physical origin of quadruple-broadband absorption is clarified by studying the electric field distributions at resonant frequencies. Finally, we investigate the effects of incidence and polarization angles on quadruple-broadband perfect absorption.

2. Design and Simulation

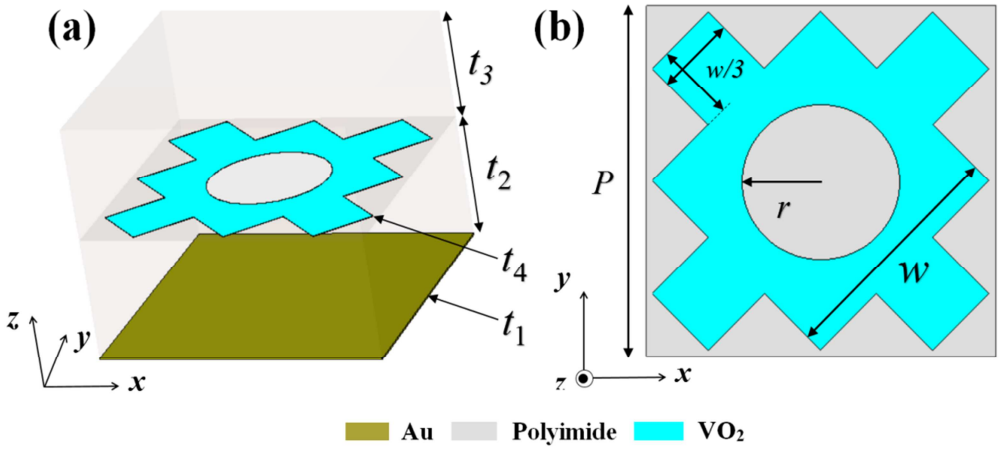

Figure 1. *Schematic diagram of the proposed absorber: (a) 3D structure of the unit cell, (b) front view of the unit cell.*

The unit cell of proposed absorber possesses the gold-polyimide-VO_2-polyimide configuration as shown in Figure 1. Such a configuration has already been validated as the efficient absorber structure in the previous studies [41, 42]. The gold ground plane has the thickness of $t_1 = 0.4$ μm and the conductivity of $\sigma = 4.561\times10^7$ S/m. The polyimide material has the dielectric constant of $\varepsilon = 3(1 + i0.06)$ [43]. The thickness of VO_2 resonator is $t_4 = 0.1$ μm and its optical dielectric constant is represented by the Drude model [44]:

$$\varepsilon(\omega)=\varepsilon_\infty-\frac{\omega_p^2(\sigma)}{\left(\omega^2+i\gamma\omega\right)} \tag{1}$$

where, $\varepsilon_\infty=12$ and $\gamma=5.75\times10^{13}$ rad/s stand for the high-frequency permittivity and the collision frequency, respectively. The plasma frequency is given as:

$$\omega_p^2(\sigma)=\frac{\sigma_{VO_2}}{\sigma_0}\omega_p^2(\sigma_0) \tag{2}$$

with $\sigma_0 = 3\times10^5$ S/m and $\omega_p(\sigma_0) = 1.4\times10^{15}$ rad/s. The conductivities of VO_2 (σ_{VO_2}) are 2×10^5 S/m and 200 S/m at $T = 350$ K and $T = 300$ K, respectively [45].

We extracted the geometrical parameters of the unit cell through the optimization process with the frequency-domain solver in a CST Microwave Studio software. In our simulations, unit cell boundary conditions are applied in x- and y- directions and open boundary condition is applied in z-direction. Moreover, the proposed absorber is exposed to normally incident transverse electric (TE) and transverse magnetic (TM) waves. The absorptivity of the proposed absorber can be expressed as $A(\omega) = 1-|S_{11}(\omega)|^2-|S_{21}(\omega)|^2$, where $|S_{11}(\omega)|^2$ and $|S_{21}(\omega)|^2$ stand for reflection and transmission, respectively. For the case of proposed absorber, transmission $|S_{21}(\omega)|^2$ is close to zero on account of the gold ground plane. Then, the absorptivity can be calculated as $A(\omega) = 1-|S_{11}(\omega)|^2$.

The main objective of optimization process is to simultaneously obtain quadruple-band absorption and broadband absorption at $T = 350$ K. We first simulated the

absorption performance of proposed absorber for different values of t_2 while other geometrical parameters remain unchanged. Figure 2(a) shows that the proposed absorber possesses four wide absorption bands with absorptivity over 90% for t_2 = 30 μm. After the thickness of polyimide substrate t_2 is selected, other geometrical parameters should be optimized by turns to further improve the quadruple-broadband absorption. Figure 2(b)-2(e) display the absorption curves of proposed absorber for different values of the thickness of polyimide substrate (t_3), periodic length of unit cell (P), side length of VO_2 resonator (w), radius of circular hole (r), respectively. Consequently, the optimized values of geometrical parameters are t_2 = 30 μm, t_3 = 28 μm, P = 70 μm, w = 47 μm, r = 15 μm.

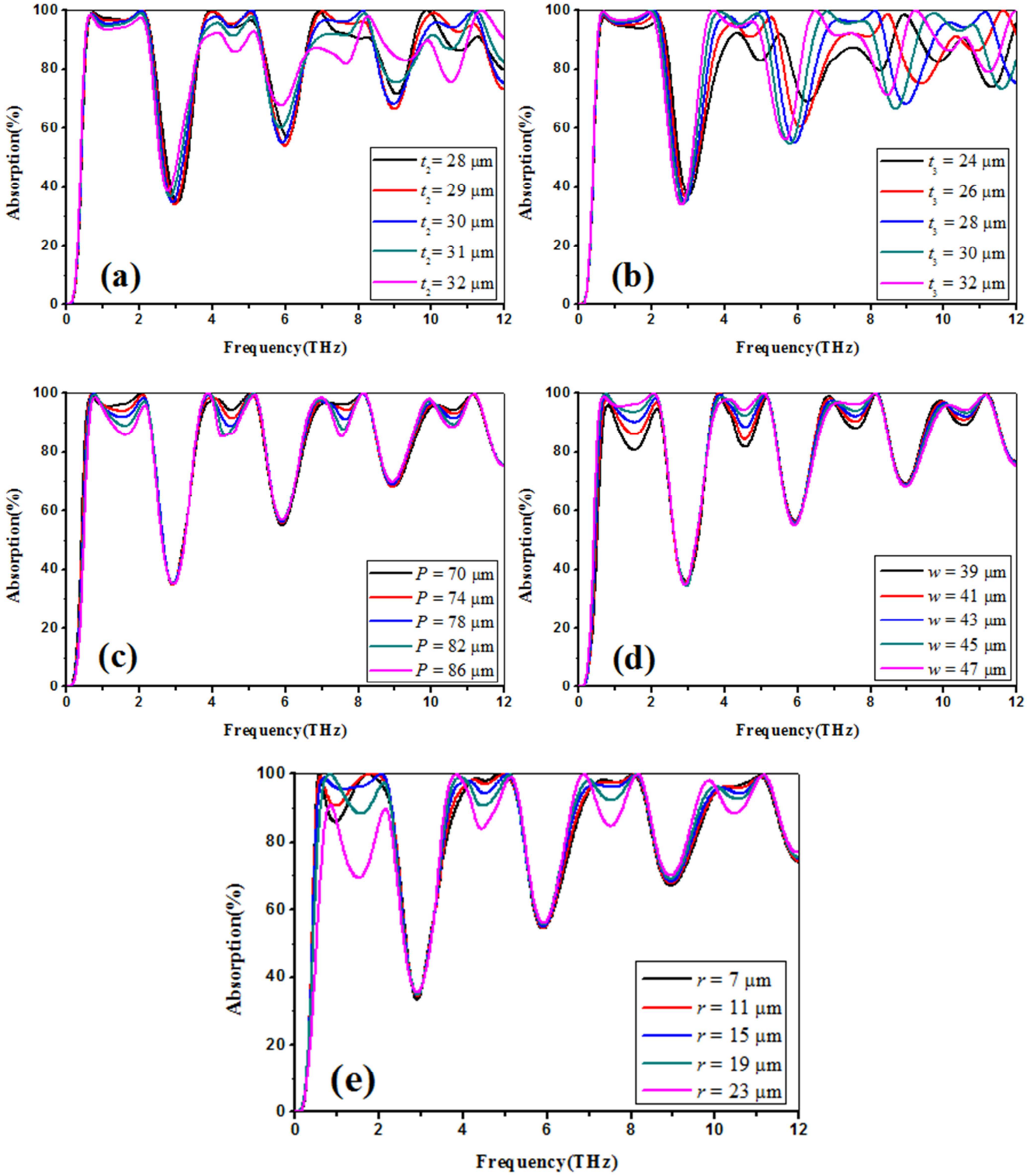

Figure 2. *Absorption curves of the proposed absorber with different geometrical parameters: (a) t_2, (b) t_3, (c) P, (d) w and (e) r.*

3. Results and Discussion

The absorption and reflection curves of the tunable quadruple-broadband THz MA with optimized geometrical parameters are plotted in Figure 3. It can be found that the proposed absorber has eight absorption peaks at 0.68 THz, 2.05 THz, 4.10 THz, 5.06 THz, 7.11 THz, 8.11 THz, 10.14 THz and 11.12 THz with absorptivites of 98.88%, 99.86%, 97.88%, 99.96%, 97.01%, 99.81, 96.01% and 99.39%, respectively. These eight absorption peaks couple together to form four broad absorption bands. The absorptivity of tunable quadruple-broadband THz MA is over 90% in four frequency ranges of 0.54-2.30 THz, 3.67-5.33 THz, 6.72-8.4 THz and 9.72-11.47 THz, and its absorption bandwidths are 1.76 THz, 1.66 THz, 1.68 THz and 1.75 THz, respectively.

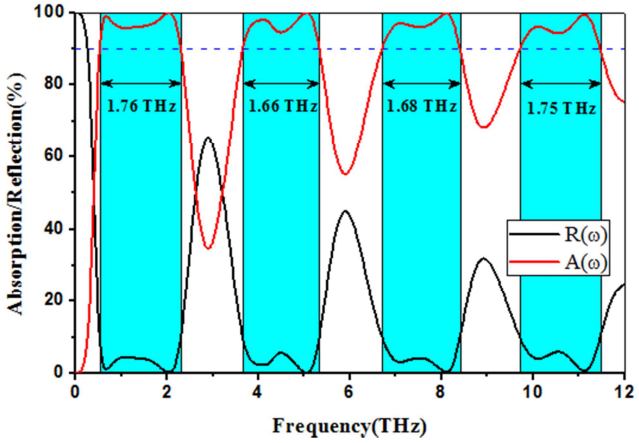

Figure 3. *Absorption and reflection curves of the proposed absorber under TE wave at T=350 K.*

The absorption tunability of proposed absorber is also investigated. The conductivity of VO_2 changes with environmental temperature. Then, since the permittivity of VO_2 is influenced by its conductivity, we are able to tune the absorptivity of proposed absorber under thermal control. As shown in Figure 4, with the increase of conductivity of VO_2, the absorptivities of four absorption bands continuously increase from 20% to 96.1%, from 47.4% to 94.3%, from 64.2% to 96% and from 73.8% to 94.6%, respectively. The modulation depth, defined as MD = $(A_m\text{-}A_i)/A_m\times100$ is a critical factor of the tunable MA, where A_m and A_i stand for the absorptivities for metallic and insulator states of VO_2, respectively [46]. This absorber possesses the modulation depths of 79.15%, 49.71%, 33.03% and 21.98% at 1.48 THz, 4.46 THz, 7.45 THz and 10.44 THz, respectively.

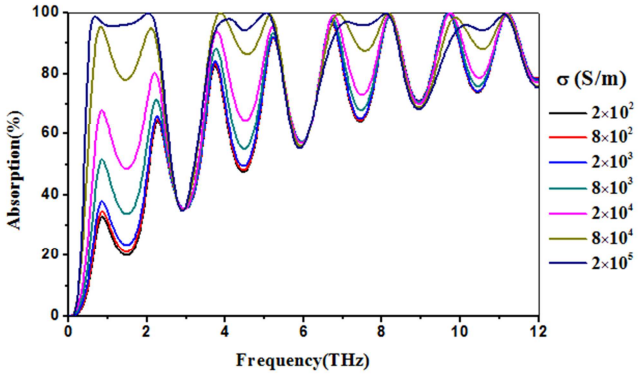

Figure 4. *Absorption curves of the proposed absorber with different conductivities of VO_2.*

Here, we compared the absorption performances of tunable quadruple-broadband THz MA with other results reported in similar studies (see Table 1). Despite the simple absorber structure as shown in Figure 1, our absorber has good tunable quadruple-broadband absorption performance. It is natural that when the number of absorption bands increases in the limited simulation frequency range of 0-12 THz, the bandwidth of each absorption band becomes narrower. So, our absorber has broad application prospects in THz modulators, sensors, switchers and detectors.

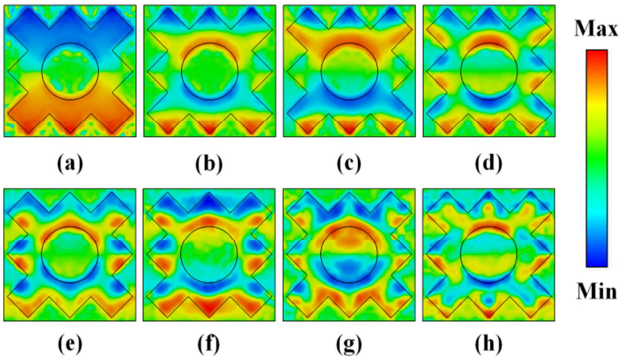

Figure 5. *Electric field (E_z) distributions at resonant frequencies: (a) f_1=0.68 THz, (b) f_2=2.05 THz, (c) f_3=4.10 THz, (d) f_4=5.06 THz, (e) f_5=7.11 THz, (f) f_6=8.11 THz, (g) f_7=10.14 THz, (h) f_8=11.12 THz.*

Table 1. *Comparison of the proposed absorber with other studies.*

Ref.	Absorption Bandwidth (THz)	Adjustable Material	Tunable Range (%)	Thickness (μm)
[38]	2.32, 2.03	VO_2	2-94	12.28
[39]	0.88, 0.77	VO_2	20-90	35.3
[40]	3.40, 3.06	VO_2	2-100	25.51
[41]	3.41, 3.25	VO_2	20-90	27.8
[42]	2.35, 2.30, 2.40	VO_2	20-90	44.4
This work	1.76, 1.66, 1.68, 1.75	VO_2	20-96	58.5

To illustrate the physical origin of quadruple-broadband perfect absorption, we studied the electric field (E_z) distributions at the eight resonant modes (f_1, f_2, f_3, f_4, f_5, f_6, f_7 and f_8). The simulated electric field (E_z) distributions on the

x-y plane are plotted in Figure 5. As shown in Figure 5(a), at f_1=0.68 THz, the strong electric field concentrates in lower and upper areas of VO_2 resonator, thus producing a dipole resonance. At f_2=2.05 THz, the electric field is strongly localized in the outer and inner edges except for left and right sides of VO_2 resonator as shown in Figure 5(b). Such a distribution produces a quadrupole resonance. Thus, the first broad absorption band is attributed to the dipole and quadrupole resonances. As shown in Figure 5(c)-5(h), at f_3=4.10 THz, f_4=5.06 THz, f_5=7.11 THz, f_6=8.11 THz, f_7=10.14 THz and f_8=11.12 THz, the electric fields are strongly distributed on the inner and outer edges of VO_2 resonator, thus generating the high-order resonances. So, the second, third, and fourth broad absorption bands originate from the combination of similar high-order resonances.

Moreover, we further investigated the physical origin of quadruple-broadband absorption by means of LC circuit resonance and standing wave resonance. In accordance with refs. [47, 48], the resonant frequency of MA is calculated as:

$$f_j \approx (2j-1)\frac{c}{2nl}, j = 1,2,3,... \quad (3)$$

where c, l, and n stand for the light speed in vacuum, the length of resonator, and the index of dielectric substrate, respectively. According to Eq. (3), the fundamental mode (j = 1) and its odd resonant modes are only valid. The absorption peaks of MA originate from these resonance modes. For example, the resonant frequency for the case of j = 2 must be 3 times greater than the resonant frequency of j = 1. Table 2 shows the resonant frequencies of the proposed absorber with different VO_2 conductivities (see Figure 4). Here, $f_{average}$ are the average values of resonant frequencies for the cases of f_1-f_8, and $f_{theoretical}$ are the theoretical frequencies calculated by Eq. (3). It can be seen from Table 2 that the average of second resonant frequencies ($f_{2,\ av}$=2.20 THz) is approximately 3 times of the average of first resonant frequencies ($f_{1,\ av}$=0.82 THz). Similarly, $f_{3,\ av}$=3.82 THz, $f_{4,\ av}$=5.19 THz, $f_{5,\ av}$=6.81 THz, $f_{6,\ av}$=8.19 THz, $f_{7,\ av}$=9.79 THz and $f_{8,\ av}$=11.20 THz are roughly five, seven, nine, eleven, thirteen and fifteen times of $f_{1,\ av}$=0.82 THz, respectively. We can also know that there are some errors between $f_{average}$ and $f_{theoretical}$. The reason is that Eq. (3) neglects the dielectric dispersion of polyimide layer. Consequently, we can conclude that the quadruple-broadband perfect absorption is attributed to the fundamental and high-order resonances of VO_2 resonator.

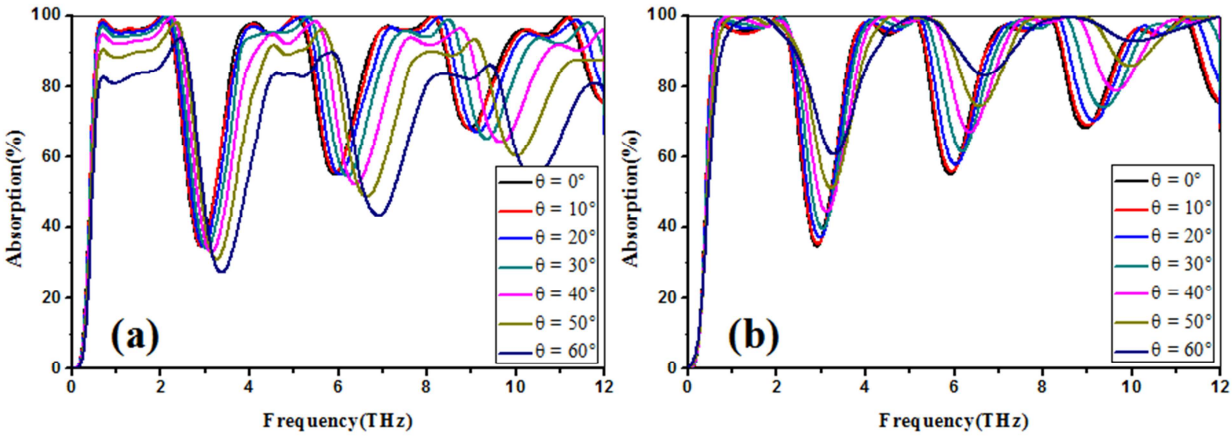

Figure 6. *Absorption curves of the proposed absorber for different values of incidence angle at (a) TE and (b) TM waves.*

Table 2. *Resonant frequencies of the proposed absorber with different values of VO_2 conductivity.*

Conductivity of VO_2 (S/m)	Resonant frequency (THz)							
	f_1	f_2	f_3	f_4	f_5	f_6	f_7	f_8
200	0.86	2.28	3.75	5.24	6.72	8.22	9.70	11.22
800	0.86	2.28	3.75	5.23	6.72	8.22	9.70	11.22
2000	0.86	2.26	3.75	5.23	6.72	8.22	9.70	11.22
8000	0.86	2.24	3.76	5.23	6.74	8.22	9.72	11.20
20000	0.85	2.21	3.79	5.20	6.76	8.20	9.75	11.20
80000	0.82	2.11	3.89	5.14	6.90	8.17	9.87	11.18
200000	0.68	2.05	4.10	5.06	7.11	8.11	10.14	11.12
$f_{average}$	0.82	2.20	3.82	5.19	6.81	8.19	9.79	11.20
$f_{theoretical}$	-	2.46	4.10	5.74	7.38	9.02	10.66	12.30

In order to examine the incidence angle dependence of tunable quadruple-broadband THz MA, we analyzed the absorption curves of proposed absorber with different incidence angles under TE and TM waves. As shown in Figure 6(a), the increase of incidence angle under TE wave results in the blue-shift of four absorption bands, but the absorptivity of each absorption band still remains over 80% for large incidence angle of 50°. Under TM wave, the increase of incidence angle also results in the blue-shift of four absorption bands as shown in Figure 6(b), but the absorptivity of each

absorption band still exceeds 90% for large incidence angles up to 60°. Thus, our absorber possesses good incidence angle stability.

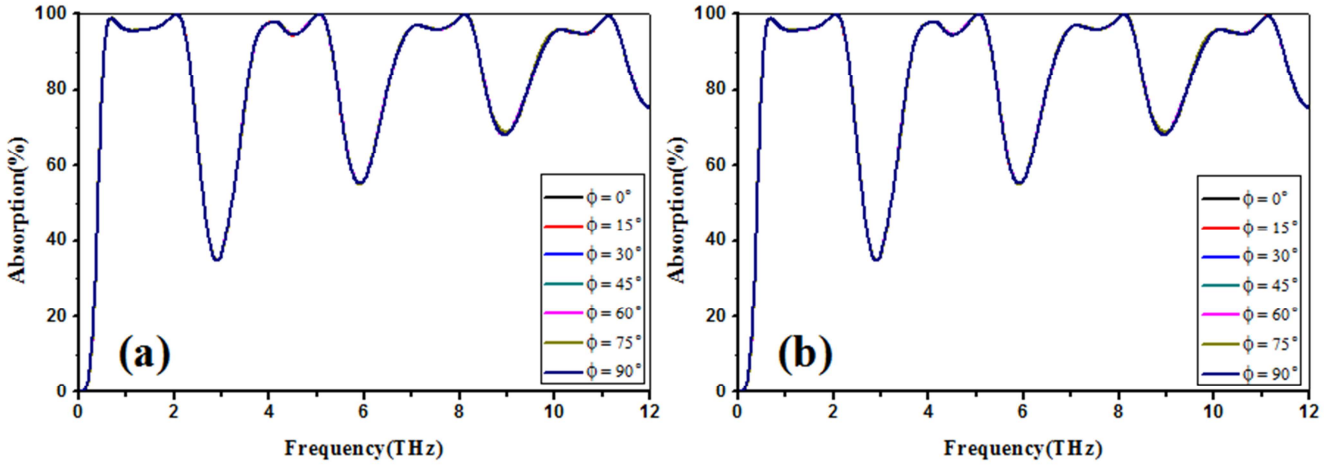

Figure 7. *Absorption curves of the proposed absorber for different values of polarization angle at (a) TE and (b) TM waves.*

Finally, we simulated the absorption performance of proposed absorber for different values of polarization angle at TE and TM waves. Our designed absorber possesses good polarization-insensitivity owing to the fourfold rotational symmetry as shown in Figure 7.

4. Conclusion

Until now, various designs on tunable dual-broadband/triple-broadband THz MAs have been proposed. However, no further research on the tunable quadruple-broadband THz MA has been done. In this work, we have proposed a simple design of tunable quadruple-broadband THz MA based on VO_2. Simulation results show that the proposed absorber has four broad absorption bands with absorptivity above 90% in frequency ranges of 0.54-2.30 THz, 3.67-5.33 THz, 6.72-8.4 THz and 9.72-11.47 THz, and the corresponding absorption bandwidths reach 1.76 THz, 1.66 THz, 1.68 THz and 1.75 THz, respectively. The absorptivities of four absorption bands can be dynamically tuned from 20% to 96.1%, from 47.4% to 94.3%, from 64.2% to 96% and from 73.8% to 94.6%, respectively. The overlap of fundamental and high-order resonances on the single VO_2 resonator results in the quadruple-broadband perfect absorption. Furthermore, the proposed absorber possesses wide incidence angle stability and polarization-insensitivity. Thus, the proposed absorber has broad application prospects in THz imaging, modulating, detecting and sensing.

Competing Interests

The authors declare no competing interests.

Author Contributions

K. J. Ri conceived the idea, performed the simulations and wrote the manuscript. D. S. Pak analyzed the results and assisted the revision of the manuscript. C. H. Ri supervised the entire project. All authors have read and approved the final manuscript.

Data Availability

All data used to support the findings in this study are included within the paper.

ORCID

Kwang-Jin Ri: https://orcid.org/0009-0002-2603-2724

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